Maunakea Spectroscopic Explorer

New series of high resolution and efficiency VPH gratings

Dispersing Elements Workshop, Milan, 9-11th Oct 2017



MSE High Resolution Survey

Maunakea Spectroscopic Explorer

- MSE will include a High Resolution mode for Galactic Archaeology.
- 11m telescope, >1000 simultaneous
 HR spectra, R=40,000, 3 bands.
- ⇒ the HR spectrograph costs form a very large fraction of the total.
- Would like to use VPHs for MSE, as for HERMES and 4MOST (efficient, tuneable, cheap, robust, Littrow).
- But as telescope sizes and resolution requirements increase, are they viable design solutions?





Beam Size



Maunakea Spectroscopic Explorer

Spectrograph cost/difficulty/risk strongly driven by the collimated beam size:

 $B = R D_T \phi_F / (2n_1 \tan \alpha_0)$

(**R** is the resolution, D_{τ} is the telescope diameter, ϕ_{F} is the angular slit width, n_{1} is the index of the immersion medium, and α_{0} is the overall grating angle)

B scales directly as **R**, **D**_T, ϕ_{F}

All fixed (unless image-slicing used)

 \Rightarrow Larger grating angle is very desirable.

But efficiency also paramount!









Maunakea Spectroscopic Explorer

Peak efficiency of VPH gratings was approximated by Kolgenik (1969):

$$\eta \approx \frac{1}{2} \sin^2 \left(\frac{\pi \Delta n_2 d}{\lambda \cos \alpha_2} \right) + \frac{1}{2} \sin^2 \left(\frac{\pi \Delta n_2 d}{\lambda \cos \alpha_2} \cos 2\alpha_2 \right)$$
(1)

(λ is the wavelength, Δn_2 is the index modulation, d the DCG thickness, α_2 is the grating angle within the DCG, and the two terms are for s and p polarizations respectively).

For each polarization, can get ~100% efficiency by choice of **d** and Δn_2 , to get $\pi/2$ within the brackets*

For highest bandwidth, normally want small d and large Δn_2



*(or **3**π**/2** or **5**π**/2** etc).

Diffraction efficiency



- For small angles, $\cos 2\alpha_2 \sim 1$, and hence excellent peak efficiency is possible in both polarizations simultaneously.
- But as α₂ increases, the cos (2α₂) term introduces a mismatch between the desired DCG properties for each polarization.





Diffraction efficiency



- For small angles, $\cos 2\alpha_2 \sim 1$, and hence excellent peak efficiency is possible in both polarizations simultaneously.
- But as α₂ increases, the cos (2α₂) term introduces a mismatch between the desired DCG properties for each polarization.





Diffraction efficiency



Simultaneous high efficiency for both polarizations is still possible for special values of α_2 , by matching an efficiency peak in the s polarization with a *different* peak in the **p** polarization. 'Dickson gratings'





Maunakea Spectroscopic Explorer

We need

$$\frac{2\pi \Delta n d}{\lambda \cos \alpha_2} = 2a+1 \quad (2) \text{ and } \cos 2\alpha_2 = \frac{2b+1}{2a+1} \quad (3) \text{ for integral } a, b$$

Simplest Dickson grating has (a,b) = (0,1), $\alpha_2 = 35.3^\circ$, $\cos 2\alpha_2 = 1/3$. Matches the 1st *p*-polarization peak with the 2nd *s*-polarization peak.

Leads to overall grating angle ~47° in air for unimmersed grating. Large overall gain for plausible angular bandwidths.







Maunakea Spectroscopic Explorer

First astronomical uses of Dickson gratings were for 6dF/RAVE on the UK Schmidt (2003) and AAOmega on the AAT (2004), both for Call triplet work (~850nm).







SuperDickson Gratings?

Maunakea Spectroscopic Explorer

- Wasatch took a patent on Dickson gratings in 2004, specifically covering **a** = **0**,**1**,**2**,**3**... and **b** = **0**,**1**,**2**,**3**...
- Obvious that *a* must be +ve, from equation (2).
- However, **b** is not so constrained, and **there are multiple families of further solutions with –ve b**.
- All these new solutions have Bragg angles > 45°. This means they all need prisms to get the light into and out of the grating while avoiding TIR.

The two most interesting new classes of gratings are (a,b) = (1,-1) and (a,b) = (0,-1).





(*a*, *b*) = (1,-1),
$$\alpha_2 = 54.7^{\circ}$$



Maunakea Spectroscopic Explorer

- Matches 1st *p* peak with
 -2nd *s* peak.
- α₀ ~48°. Gives a dispersion ~50% larger than a classic unimmersed Dickson grating.
- DCG parameters look ok e.g. 5378 lines/mm, n₂=1.35±0.15, d = 2.37μm.



- The FWHM bandwidth is 6.4% in wavelength, or 0.16 rad (9°) in angle – useable but a bit narrower than we'd like.
- Referred to by Baldry *et al* (2004).



$$(a, b) = (0, -1), \alpha_2 < 20^{\circ}$$



 $\alpha_2 = 90^\circ$ is unphysical, but as $\alpha_2 \rightarrow 90^\circ$, 1st s and -1st p peaks become phased. Design shown has $\alpha_0 \sim 65^\circ$,

Design shown has $\alpha_0 \sim 65^\circ$, $\alpha_2 = 72^\circ$, 6445 lines/mm, $d = 1\mu m$, $n=1.4\pm0.075$

FWHM bandwidth is 3.7%, 0.22rad, 12.5°, very nice!



The DCG is thinner than used in gratings to date, but the modulation is modest.

Larger angles possible but DCG thickness becomes even thinner.

2nd polarization comes 'for free' – almost no loss of bandwidth



Implications for Spectrograph design

MSE HR spectrographs require $\mathbf{R} \sim 40,000$ in two arms (~409nm, ~481nm) each with $\Delta \lambda / \lambda \sim 1/30$. Telescope is 11m, fiber size 0.8" or FWHM 0.69".

- If classic Dickson gratings used, beam size is 700mm!
- New (1,-1) grating, still 450mm.
- But with (0,-1) grating, **B**=240mm.
- 240mm is feasible for KOSI
- Camera optics sizes not too scary, largest lenses 300mm (vs 450mm in NIAOT CoDR design).



Dispersion Module - R

Dispersion Module - G

MSE

design



Dispersion Module





Camera Detector